

# An Approximate Likelihood Ratio Detector for QTMS Radar and Noise Radar

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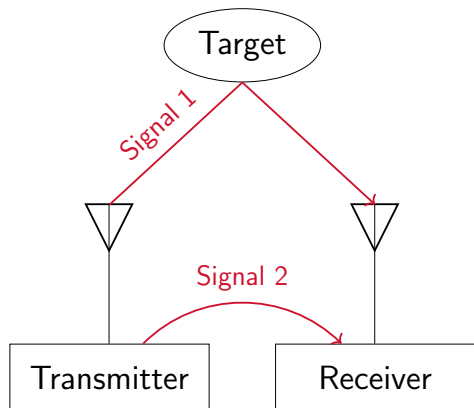
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# Introductory remarks

- ▶ Radar stands for **radio detection and ranging**
- ▶ Modern radars support **many more functions** than just detection and ranging, but these are still basic capabilities of radars
  - ▶ Other functions include target tracking, clutter suppression, synthetic aperture radar, and many more
- ▶ In this presentation, we focus on the **detection** aspect

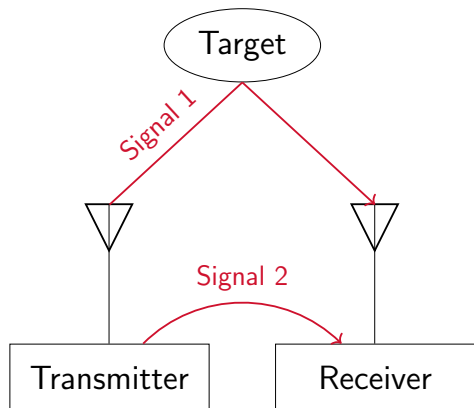
# (Generalized) matched filtering



We consider radars that work as follows:

1. Produce two microwave signals.
2. Transmit one. Keep the other.
3. Receive and measure a signal.
4. Use the received and retained signals to decide whether there is a target.

# (Generalized) matched filtering



- ▶ This is essentially **matched filtering**
- ▶ However, it is **more general** than the strict definition of the matched filter,  $h[n] = x^*[-n]$ 
  - ▶ Reference signal need not be exactly the same as the transmit signal
  - ▶ Filter need not be linear

# The radar detection problem

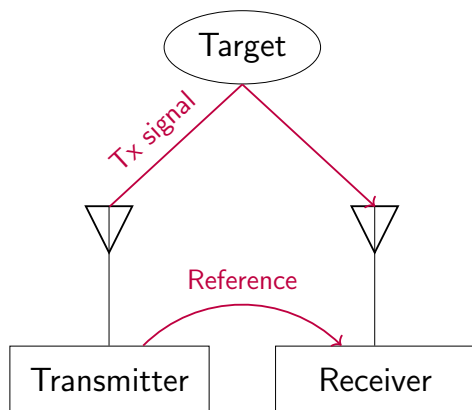
- ▶ As far as detection is concerned, radars are machines for **hypothesis testing**
- ▶ We wish to distinguish between:

$H_0$  : Target absent

$H_1$  : Target present

- ▶ We need a **test statistic**—that is, a **detector function**—to distinguish between  $H_0$  and  $H_1$
- ▶ Choice of detector function depends on the exact nature of the radar signals

# Noise radar



My research focuses on **noise radars** which work like this:

1. Produce a microwave **noise** signal.
2. Transmit the signal, retaining a copy as a reference.
3. Receive a signal from free space.
4. Correlate the received signal with the reference.

# Mathematical background

- ▶ RF signals are described by a pair of real-valued time series:  
**in-phase voltages**  $I(t)$  and **quadrature voltages**  $Q(t)$
- ▶ For a noise radar, we consider two signals (four time series):
  - ▶ received signal:  $I_1(t)$  and  $Q_1(t)$
  - ▶ reference signal:  $I_2(t)$  and  $Q_2(t)$
  - ▶ Note: no need to consider the *transmitted* signal
- ▶ For noise radar, each signal is a **random process**
- ▶ We assume that all the signals are Gaussian white noise (so we can drop the time variable  $t$ )

# The noise radar covariance matrix

$$\begin{bmatrix} \sigma_1^2 & 0 & \rho\sigma_1\sigma_2 \cos \phi & \rho\sigma_1\sigma_2 \sin \phi \\ 0 & \sigma_1^2 & -\rho\sigma_1\sigma_2 \sin \phi & \rho\sigma_1\sigma_2 \cos \phi \\ \rho\sigma_1\sigma_2 \cos \phi & -\rho\sigma_1\sigma_2 \sin \phi & \sigma_2^2 & 0 \\ \rho\sigma_1\sigma_2 \sin \phi & \rho\sigma_1\sigma_2 \cos \phi & 0 & \sigma_2^2 \end{bmatrix}$$

- ▶ It can be shown that  $I_1$ ,  $Q_1$ ,  $I_2$ ,  $Q_2$  are characterized by the above covariance matrix
- ▶  $\sigma_1^2$ ,  $\sigma_2^2$  are signal powers for the received and reference signals;  $\phi$  is the phase between them

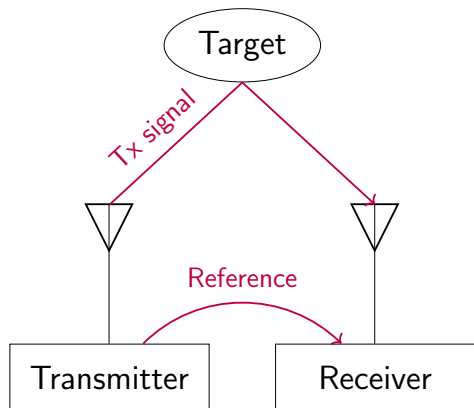


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- ▶ It can be shown that  $I_1$ ,  $Q_1$ ,  $I_2$ ,  $Q_2$  are characterized by the above covariance matrix
- ▶  $\sigma_1^2$ ,  $\sigma_2^2$  are signal powers for the received and reference signals;  $\phi$  is the phase between them
- ▶  $\rho$  characterizes the **correlation** between the two signals

# The importance of $\rho$

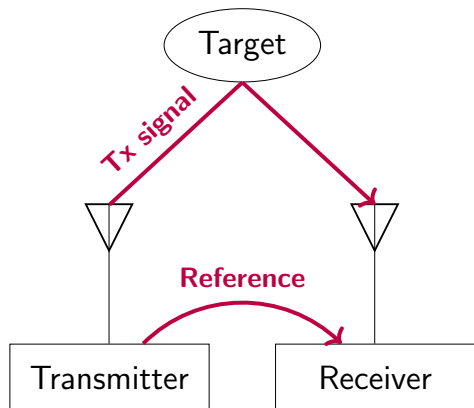


- ▶  $\rho$  tells us whether there is any **correlation** between the received and reference signals
- ▶  $\rho > 0$  at receiver  $\implies$  target **present**
- ▶  $\rho = 0$  at receiver  $\implies$  target **absent**
- ▶ Target detection problem = **hypothesis testing on  $\rho$**

## Why introduce $\rho$ ?

- ▶  $\rho$  has previously been little-studied in the context of radars
- ▶ Not as familiar as SNR
- ▶ One advantage: the target detection problem is easily formulated as a hypothesis test in terms of  $\rho$
- ▶  $\rho$  takes into account **imperfections in the reference signal**, which is ignored when we deal only with SNR
  - ▶ We will return to this point when we discuss *quantum two-mode squeezing radar*

# Hypothesis testing on $\rho$



- ▶ Recall:  $\rho$  tells us the **correlation** between the received and reference signals
- ▶ In terms of  $\rho$ , the target detection problem requires us to distinguish between these hypotheses:

$H_0 : \rho = 0$  Target absent

$H_1 : \rho > 0$  Target present

# A note about choosing hypotheses

$H_0 : \rho = 0$  Target absent

$H_1 : \rho > 0$  Target present

- ▶ Note that  $H_1$  is a **composite** hypothesis
- ▶ We **do not know** what  $\rho$  would be if a target is present
  - ▶  $\rho$  is a function of range, radar cross section, background noise, ...
- ▶ We are **not** testing between  $\rho = 0$  and  $\rho = \kappa$  for some known value of  $\kappa$
- ▶ The Neyman-Pearson lemma does not apply here

# Detector functions

- ▶ There are many detector functions which could be used for this target detection problem
- ▶ A detector function is used for radar detection as follows:
  1. Set a **threshold**
  2. Calculate the detector function using the given  $I_1$ ,  $Q_1$ ,  $I_2$ , and  $Q_2$  samples
  3. **Declare a detection** if the value exceeds the threshold
- ▶ One natural detector function: **the (generalized) likelihood ratio**

# Nuisance parameters

$$\begin{bmatrix} \sigma_1^2 & 0 & \rho\sigma_1\sigma_2 \cos \phi & \rho\sigma_1\sigma_2 \sin \phi \\ 0 & \sigma_1^2 & -\rho\sigma_1\sigma_2 \sin \phi & \rho\sigma_1\sigma_2 \cos \phi \\ \rho\sigma_1\sigma_2 \cos \phi & -\rho\sigma_1\sigma_2 \sin \phi & \sigma_2^2 & 0 \\ \rho\sigma_1\sigma_2 \sin \phi & \rho\sigma_1\sigma_2 \cos \phi & 0 & \sigma_2^2 \end{bmatrix}$$

- ▶ Unfortunately, the covariance matrix has three nuisance parameters:  $\sigma_1$ ,  $\sigma_2$ , and  $\phi$
- ▶ In order to simplify our problem, we assume  $\sigma_1 = 1$ ,  $\sigma_2 = 1$ , and  $\phi = 0$
- ▶ Future work: estimate these parameters or deal with them in a more principled manner

# The (simplified) noise radar target detection problem

Given  $N$  samples of the radar signals  $I_1$ ,  $Q_1$ ,  $I_2$ , and  $Q_2$  such that

$$\begin{bmatrix} I_1 \\ Q_1 \\ I_2 \\ Q_2 \end{bmatrix} \sim \mathcal{N} \left( \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}, \begin{bmatrix} 1 & 0 & \rho & 0 \\ 0 & 1 & 0 & -\rho \\ \rho & 0 & 1 & 0 \\ 0 & -\rho & 0 & 1 \end{bmatrix} \right),$$

decide which of the following is true:

$H_0 : \rho = 0$  Target absent

$H_1 : \rho > 0$  Target present



# The GLR detector

$$D_{\text{GLR}} = N \left[ \frac{2\bar{D}_1 \hat{\rho} - \bar{P}_{\text{tot}} \hat{\rho}^2}{1 - \hat{\rho}^2} - 2 \ln(1 - \hat{\rho}^2) \right]$$

- ▶  $P_{\text{tot}} \equiv I_1^2 + Q_1^2 + I_2^2 + Q_2^2$
- ▶  $D_1 \equiv I_1 I_2 - Q_1 Q_2$
- ▶ Line over expression = sample mean over  $N$  samples
- ▶  $\hat{\rho}$  = maximum likelihood estimate of  $\rho$  (complicated)

## Approximate GLR detector

$$D_{\text{GLR}} = N \left[ \frac{2\bar{D}_1\hat{\rho} - \bar{P}_{\text{tot}}\hat{\rho}^2}{1 - \hat{\rho}^2} - 2 \ln(1 - \hat{\rho}^2) \right]$$

- ▶ This is very complicated
- ▶ But to second order in  $\rho$ , this reduces to

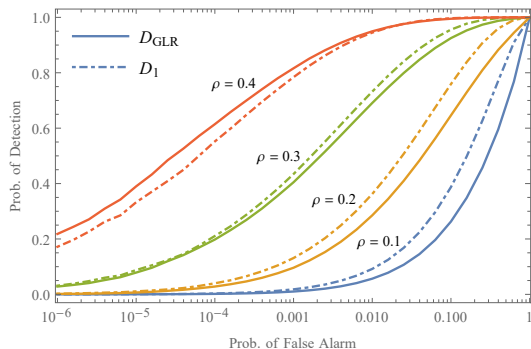
$$D_{\text{GLR}} \approx \frac{N\bar{D}_1^2}{\bar{P}_{\text{tot}} - 2}$$

- ▶ Much simpler to calculate (e.g. on a digital signal processor)
- ▶ Can obtain closed-form formula for the ROC curve

## Connection to a previous detector

- ▶  $D_1 = I_1 I_2 - Q_1 Q_2$  has itself been used as a detector function
- ▶ It was called “Detector 1” in the world’s first journal paper on experimental microwave quantum radar
  - ▶ D. Luong, C. W. S. Chang, A. M. Vadiraj, A. Damini, C. M. Wilson and B. Balaji, “Receiver Operating Characteristics for a Prototype Quantum Two-Mode Squeezing Radar,” *IEEE Transactions on Aerospace and Electronic Systems*, vol. 56, no. 3, pp. 2041-2060, June 2020 (accepted Sept. 2019)
- ▶ It is equivalent to the “digital receiver” in the world’s second journal paper on experimental microwave quantum radar
  - ▶ S. Barzanjeh, S. Pirandola, D. Vitali, and J. M. Fink, “Microwave quantum illumination using a digital receiver,” *Science Advances*, vol. 6, no. 19, p. eabb0451, May 2020 (accepted Feb. 2020)

# ROC curve comparison



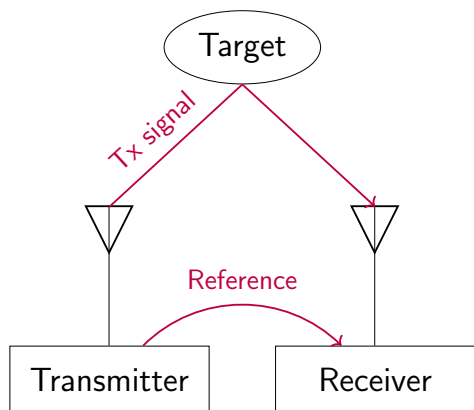
- ▶  $\rho = 0.1, 0.2, 0.3, 0.4$
- ▶  $N = 50$

- ▶ Performance of  $D_{GLR}$  is similar to  $D_1$
- ▶  $D_1$  slightly better when  $\rho$  is small;  $D_{GLR}$  better when  $\rho$  is slightly larger
- ▶ Neither one is “optimal”
- ▶ As expected, overall radar performance improves as  $\rho$  increases

# What happened to **quantum** radar?

- ▶ So far, I have spoken only about **noise radar**
- ▶ What happened to *quantum two-mode squeezing* (QTMS) radar?

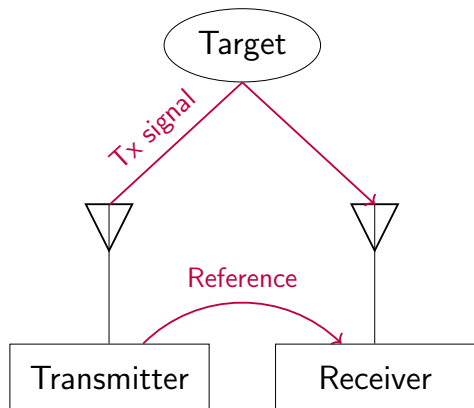
# Noise radar recap



My research focuses on **noise radars** which work like this:

1. Produce a microwave noise signal.
2. Transmit the signal, retaining a copy as a reference.
3. Receive a signal from free space.
4. Correlate the received signal with the reference.

# QTMS radar



**Quantum two-mode squeezing radars** work (roughly) like this:

1. Produce a microwave noise signal.
2. Transmit the signal, retaining a **better** copy as a reference.
3. Receive a signal from free space.
4. Correlate the received signal with the reference.

## A better reference signal

$$\begin{bmatrix} \sigma_1^2 & 0 & \rho\sigma_1\sigma_2 \cos \phi & \rho\sigma_1\sigma_2 \sin \phi \\ 0 & \sigma_1^2 & -\rho\sigma_1\sigma_2 \sin \phi & \rho\sigma_1\sigma_2 \cos \phi \\ \rho\sigma_1\sigma_2 \cos \phi & -\rho\sigma_1\sigma_2 \sin \phi & \sigma_2^2 & 0 \\ \rho\sigma_1\sigma_2 \sin \phi & \rho\sigma_1\sigma_2 \cos \phi & 0 & \sigma_2^2 \end{bmatrix}$$

- ▶ Mathematically (but not experimentally!), QTMS radars are exactly the same as noise radars except that they achieve **higher values of  $\rho$**
- ▶ The reference signal is a **higher-fidelity copy** of the transmit signal

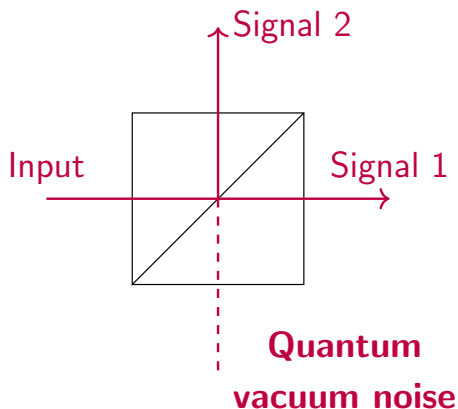


## Noise in the reference signal

- ▶ Conventional matched filtering assumes **a perfect copy of the Tx signal is available**
- ▶ Quantum mechanics says a perfect copy is **impossible**
- ▶ There will **always be noise** in  $I$  and  $Q$  voltage measurements, even in an **theoretically ideal** system

If you think you can achieve 100% correlation,  
**you've forgotten about quantum mechanics!**

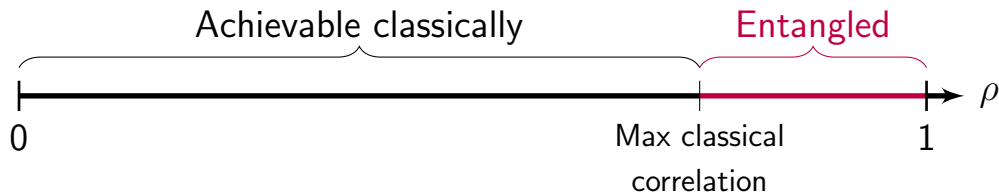
# Can't you just split the signal?



- ▶ **Vacuum noise** will creep into the beamsplitter, even at absolute zero and in a perfect vacuum

# Quantum noise and entanglement

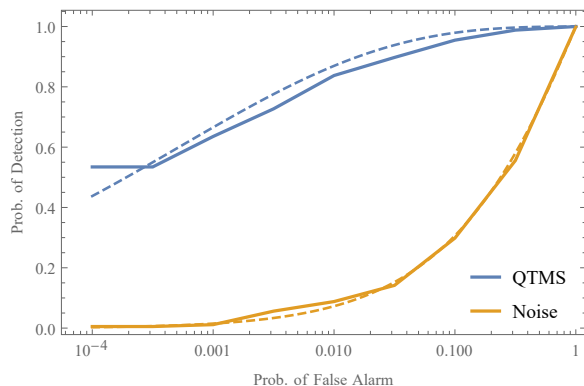
- ▶ 100% correlation is **impossible** according to quantum mechanics
- ▶ With conventional methods of preparing a reference signal,  $\rho < \text{classical limit}$
- ▶ Using **entanglement**, can achieve  $\text{classical limit} < \rho < 1$



# Radars are not made out of paper

- ▶ No amount of theory can replace an experiment
- ▶ If a radar cannot improve  $\rho$  for the same signal power, **no point pursuing it**
- ▶ A QTMS radar experiment was performed by Wilson et al. at the Institute for Quantum Computing (University of Waterloo)
  - ▶ D. Luong, C. W. S. Chang, A. M. Vadiraj, A. Damini, C. M. Wilson and B. Balaji, "Receiver Operating Characteristics for a Prototype Quantum Two-Mode Squeezing Radar," *IEEE Transactions on Aerospace and Electronic Systems*, vol. 56, no. 3, pp. 2041-2060, June 2020

# Experimental ROC curves



- ▶ Experimental ROC curves fit our theoretically derived ROC curves very well
- ▶ Improvement in QTMS radar over standard noise radar corresponds to **increasing  $\rho$  by a factor of 3**

# Conclusion

- ▶ Noise radar performance is characterized by the correlation coefficient  $\rho$  between the transmit and reference signals
- ▶ Can use the **generalized likelihood ratio** to distinguish between  $\rho = 0$  and  $\rho > 0$
- ▶ An approximate GLR works well in most cases
- ▶ QTMS radars improve performance by increasing  $\rho$
- ▶ This improvement has been **experimentally** demonstrated